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# A recoil separator for nuclear astrophysics SECAR

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## Abstract

A recoil separator SECAR has been designed to study radiative capture reactions relevant for the astrophysical rp-process in inverse kinematics for the Facility for Rare Isotope Beams (FRIB). We describe the design, layout, and ion optics of the recoil separator and present the status of the project.

## Keywords

Recoils mass separator; Wien filter; Radiative  $\gamma$ ,  $\alpha$ , and p capture.

## I. Introduction

The explosive nuclear burning of hydrogen at high temperatures and densities on the surface of accreting white dwarfs and neutron stars gives rise to a number of observable nuclear explosions including Novae [1] or X-ray bursts [2]. Recent astronomical observations provide unprecedented information, for example, on atomic abundances in Nova ejecta and time structure in X-ray bursts. Interpretation of these data requires an understanding of the nuclear processes during the explosive events and, therefore, information on the reactions of unstable, proton-rich nuclei with hydrogen and helium.

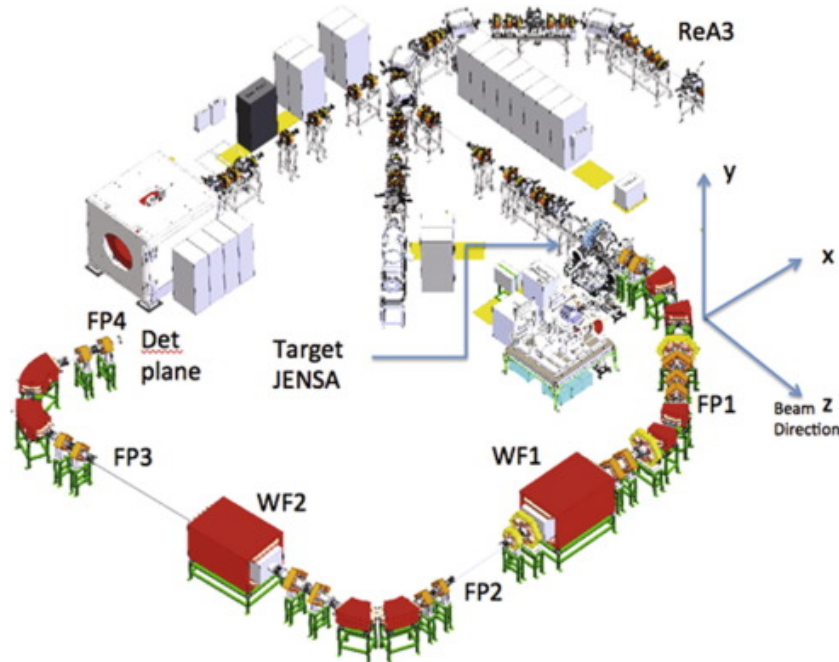
We developed SECAR (SEparator for CAPture Reactions), a recoil separator with the sensitivity needed to measure very low ( $p, \gamma$ ) and ( $\alpha, \gamma$ ) rp-process reaction rates directly at astrophysical energies in inverse kinematics for target mass from  $A = 15$  to  $A = 65$ . This requires a large angle acceptance of  $\pm 25$  mrad given by the  $^{15}\text{O}(\alpha, \gamma)^{19}\text{Ne}$  reaction at 0.5 MeV center of mass energy to accommodate the kinematic angle cone and the angle spread due to multiple scattering in the windowless gas target, so that all recoils are transmitted. The very high mass resolving power  $m/dm \geq 750$  is given by the  $^{65}\text{As}(p, \gamma)^{66}\text{Se}$  reaction and is more than a factor of 2 larger compared to existing recoil separators to achieve a beam rejection of about  $10^{-13}$ . An additional rejection of about  $10^{-4}$  is provided by the detector system.

SECAR is designed to be a next-generation device, with specifications to match the beam production capabilities of FRIB and the scientific needs of the community. These specifications will significantly exceed the two major separators in the field, the Detectors of Recoils And Gammas of Nuclear reactions (DRAGON)[4] at TRIUMF ISAC and the Daresbury Recoil Separator (DRS)[5] at ORNL. The viability of measuring proton capture reactions in inverse kinematics with a recoil separator was demonstrated in 1991 with a small system at Caltech[6]. In addition to DRAGON and DRS other separators have been built for this technique, including ARES [7], ERNA [8], and St. George [9]. SECAR will initially operate at the ReA3 rare isotope (RI) beam facility at NSCL, MSU, taking advantage of its unique capability to produce a wide range of radioactive beams. SECAR will achieve its full potential with the intense radioactive beams that can be produced at the Facility for Rare Isotope Beams (FRIB), a next generation facility currently under construction at Michigan State University.

## II. Design of the recoils separator

The floor plan of the recoil separator SECAR is shown in Fig. 1. The system consists of four sections: 1 Introduction, 2 Design of the recoils separator, 3 Ion optics, 4 Project status with four focal planes (FP1– FP4) at the end of each section. Section 1 starts at the windowless gas jet target JENSA [3] and ends at focal plane F1. JENSA is already constructed and installed and is presently used as stand alone facility. Only minor modifications are needed to adapt JENSA for the use with SECAR. Sufficiently high dispersion at FP1 is provided to select a single charge state of the beam and reaction products or recoils. Section 2 with velocity filter WF1 has a mass resolving power of about  $m/dm = 750$  that is reduced to about  $m/dm = 500$  by higher order aberrations. To achieve this there is an achromatic focus at FP2 where the beam and recoils are separated. Most of the beam is stopped while the recoils, still riding on a tail of the beam,

will be fully transmitted through Section 3. This section includes a second velocity filter increasing the mass resolving power to the required  $m/dm = 750$ . In the focal plane F3 the tail of the beam is further separated from the recoils and stopped by a slit. The final Section 4 has two functions (a) to reduce background and (b) to prepare the beam for full transmission through the detector system. The background consists of beam particles scattered from upstream beam apertures, scattering and charge exchange from the residual gas, and beam tails. The complete system consists of 2 velocity filters, 8 dipole, 14 quadrupole, 3 hexapole, and 1 octupole magnets. In addition there is a combined function magnet (Q1 + Hex) that includes a quadrupole and hexapole at the very beginning of the system.

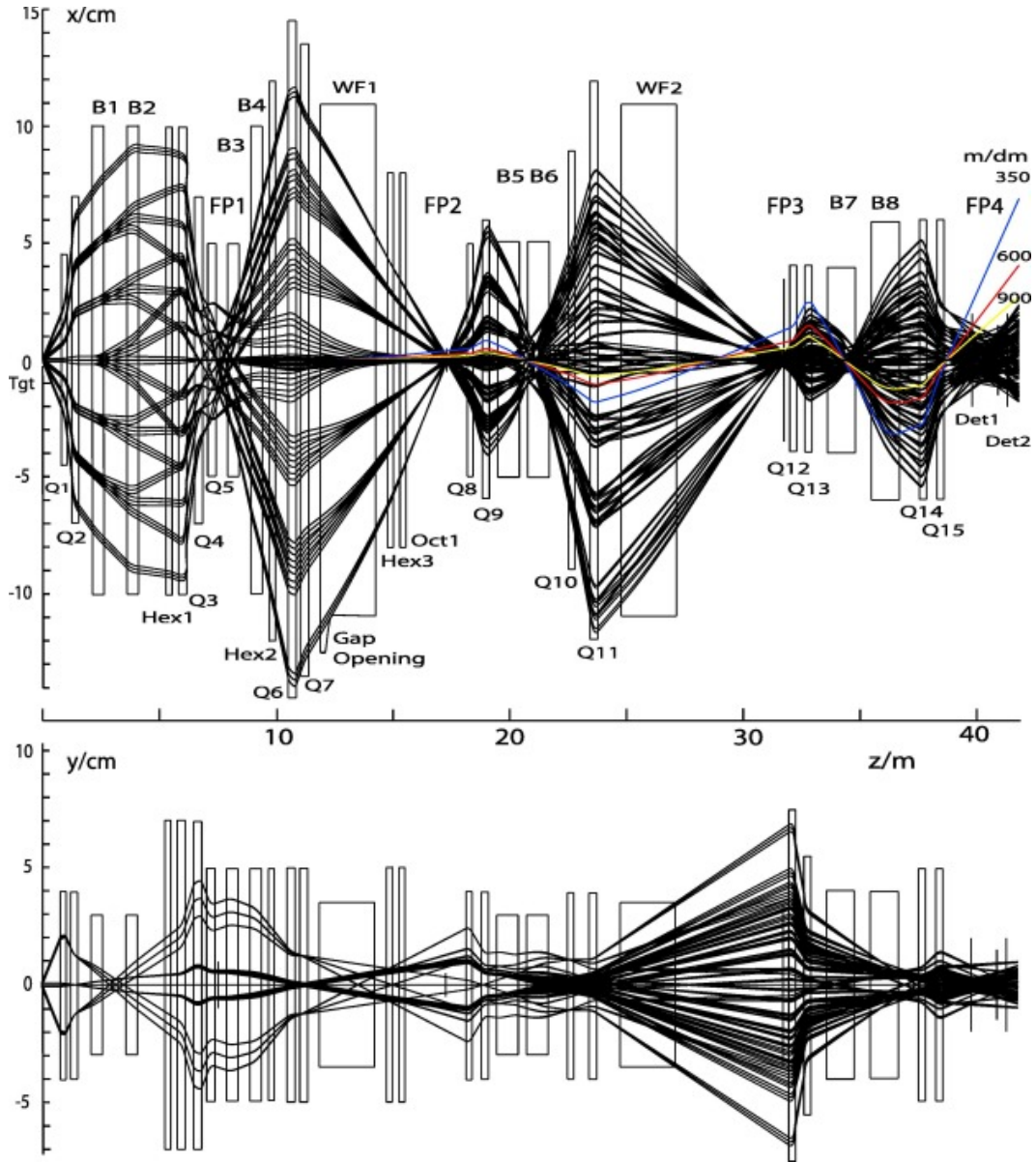


**Fig. 1.** SECAR layout in the ReA3 Hall at MSU. The beam enters the hall from the top right, impinges on the JENSA gas jet target. The recoils and unreacted projectiles enter the first section that selects a single charge state. Two additional sections each have a velocity filter (WF1, WF2) for projectile rejection. The final “cleanup” section features two dipoles and a drift section before the recoils enter the focal plane detection system.

### III. Ion optics

One of the critical design parameters of SECAR is the high mass resolving power. The ion-optical concept was developed and optimized using the code COSY Infinity [10]. The first-order mass resolving power is defined by  $R_m = R_{17}/(R_{11} \cdot 2x_0)$  where  $R_{17}$  is the mass dispersion,  $R_{11}$  the magnification and  $2x_0$  the full object spot size. However, a mass resolving power as high as  $R_m$  is only achieved if the higher order (HO) aberrations are corrected to negligible contributions. Ideally, the minimization of the image spot size including HO aberrations would be performed using a large number of rays with realistic image phase space distribution. Since this is not practical mainly because of the long computing time, we defined an array of 189

“characteristic rays” to derive the image size, as a compromise. These rays cover the maximum design acceptances in an equal-distance grid-type distribution of the horizontal ( $\pm 25$  mrad), vertical ( $\pm 25$  mrad), and energy acceptances ( $\pm 3.1\%$ ) as well as horizontal and vertical target spot sizes of  $\pm 0.75$  mm. The image size is defined as the maximum of distances between all 189 rays in the horizontal plane. A comparison of the image sizes of the optimized ion-optics using this method and Monte Carlo calculations with  $10^4$  rays with Gaussian phase-space distributions showed reasonable agreement. The ion-optical concept of SECAR was optimized sequentially for orders 1, 2, 3 and 4. This is accomplished by using appropriate shapes of the dipole magnet entrances and exit edges. In addition 3 hexapole and 1 octupole magnets are included in Section 2 for further improvement and flexibility. The inclusion of orders 5 and 6 do not change or improve the ion-optics significantly, notably the mass resolving power. The results of the final, optimized ion-optics calculation are shown in Fig. 2. In addition to the characteristic rays, rays representing mass resolving powers of 350, 600 and 900 are shown. Notice the left–right asymmetry in 2 Design of the recoils separator, 3 Ion optics owing to the HO aberrations. The specifications of the magnets and other system components like dimensions, good field regions, etc. are derived from the optimized ion-optics.



**Fig. 2.** The ion optics of SECAR for the layout shown in Fig. 1. Shown are 189 characteristic rays in the horizontal and vertical planes in the upper and lower panel, respectively. The horizontal mass resolving power is 508 at FP2 and 767 at FP3.

#### IV. Project status

SECAR is designed to allow construction in two phases. Phase 2 is the complete system as described above. In Phase 1 Section 3 with Wien filter WF2 is omitted. In this configuration Section 4 follows immediately Section 2. This is still a complete recoil separator but with a reduced mass resolving power of  $\approx m/dm = 500$  instead of the design goal of 750. This would limit the mass range that can be studied to  $\approx A < 40$ . At present SECAR Phase 1 is funded, but we will apply for additional funds to be able to construct the full Phase 2 system. Based on the conceptual design report, requests for quotations with manufacturing specifications have been produced and were sent to potential manufacturers. Quotations have

been received and a vendor has been selected. SECAR is scheduled to become operational in 2021.

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